

1 The approach towards the ball, rather than the physical characteristics of the kicker, limits
2 accurate rugby place kicking range
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40 **The approach towards the ball, rather than the physical characteristics of the**
41 **kicker, limits accurate rugby place kicking range**

42
43 **Abstract**

44
45 The aim of this study was to understand how a place kicker's range is limited by their approach
46 to the ball and their physical characteristics. Thirty-three kickers performed maximal place
47 kicks and vertical jumps in a laboratory. Whole-body motion and ground reaction forces during
48 the approach phase of the kicks, jump performance and anthropometric measurements of those
49 whose predicted *maximum distance* was limited by range ($n = 17$) rather than accuracy were
50 analysed. Principal component analysis (PCA) reduced the number of variables considered
51 before stepwise regression analyses assessed variance in place kick *maximum distance* and
52 associated criteria. Four components, explaining 94% of the variance in *maximum distance*,
53 were extracted from the PCA: width of approach, anterior-posterior body position, centre-of-
54 mass height and lower limb strength. Lower limb strength was a significant predictor of both
55 kicking foot velocity ($R^2 = 0.55, p = 0.001$) and ball velocity magnitude ($R^2 = 0.57, p < 0.001$).
56 However, *maximum distance* was determined by body position during the approach (antero-
57 posterior position, $R^2 = 0.52, p = 0.001$ and centre-of-mass height, $R^2 = 0.12, p = 0.049$). This
58 highlights the importance of considering three-dimensional motion of the kicker alongside their
59 physical capabilities to understand place kicking range.

60
61 **Keywords:** anthropometrics, ground reaction forces, kinematic, lower-body, strength

62
63
64 **Introduction**

65
66 Place kicks (conversions and penalties) contributed 45% of all points scored in international
67 matches over a 10-year period (Quarrie & Hopkins, 2015). Understanding how successful place
68 kicking is achieved is therefore desirable in order to improve the likelihood of team success.
69 To-date the majority of research has focussed on the kicking phase (from the top of the
70 backswing to ball contact) and has concentrated on the motion of the kicking leg, identifying
71 hip flexion and knee extension motion as key determinants of foot and ball velocity (Atack et
72 al., 2019b; Padulo et al., 2013; Sinclair et al., 2014; Sinclair et al., 2017; Zhang et al., 2011)
73 and kick accuracy (Atack et al., 2019b; Sinclair et al., 2017), as well understanding the
74 influence of the kicking foot swing plane on kick accuracy (Bezodis et al., 2019). Motion of
75 the torso has been found to influence both ball velocity, through greater longitudinal trunk and
76 pelvis rotations (Atack et al. 2019b; Bezodis et al., 2007; Green et al., 2016) and kick accuracy,
77 with a greater pelvis-trunk separation and longitudinal trunk rotation considered detrimental to
78 performance (Atack et al., 2019b; Hébert-Losier et al., 2020). The non-kicking-side arm also
79 rotates across the body during the downswing to counteract the angular momentum of the
80 kicking leg and maintain a more accurate kick (Bezodis et al., 2007).

81
82 The movement of the kicker prior to the kicking phase has received limited attention within
83 the literature despite the importance placed on it by coaches (Bezodis & Winter, 2014). Place
84 kickers adopt an angled approach to the ball of $34 \pm 6^\circ$ (Bezodis et al., 2017), consistent with
85 soccer instep kicking (Lees et al., 2009), and position their support foot ~ 0.30 m lateral to, and
86 ~ 0.10 m behind, the ball (Bezodis et al., 2017; Cockroft & van den Heever, 2016). This support
87 foot position has demonstrated relatively low inter- and intra-kicker variation in place kicking
88 (Bezodis et al., 2017; Cockroft & van den Heever, 2016) and despite it being the base of
89 support, about which the kicking leg swings, even extreme (± 0.30 m) manipulations in this

90 position had no effect on ball velocity (Baktash et al., 2009). These findings are supported by
91 experimental manipulations to approach angle in soccer instep kicking, which revealed
92 minimal effects on both ball velocity and accuracy (Kellis et al., 2004; Isokawa & Lees, 1988;
93 Scurr & Hall, 2009).

94
95 Evidence from soccer instep and Australian Rules punt kicking has, however, identified a
96 positive association between approach velocity and the kicking foot and ball velocities
97 achieved (Andersen & Dörge, 2011 and Ball, 2008). It has been suggested that a faster
98 approach may enable a longer final step (Ball, 2008), and thus a longer flight time to achieve
99 greater kicking leg retraction at the top of the backswing and subsequently a longer kicking
100 foot path towards ball contact (De Witt, 2002). Furthermore, if the length of the final step and
101 position of the kicking foot at the top of the backswing enable a faster kicking foot velocity, it
102 is also important to consider the anthropometric characteristics (e.g. lower limb lengths) of the
103 kicker given the inherent influence they may have.

104
105 A second advantage that a fast approach may provide a kicker is the ability to transfer the
106 forward whole-body momentum to angular momentum of the kicking leg, as demonstrated in
107 soccer instep kicking (Potthast et al, 2010). Decelerating this forward momentum, through
108 exertion of large posterior ground reaction forces (GRFs) by the support leg, will enable a
109 kicker to transfer this forward velocity to the kicking leg and also to reduce their centre of mass
110 (CM) velocity at ball contact (BC), where a faster velocity has previously been found to
111 negatively affect within-kicker place kick performance (Hébert-Losier et al., 2020). The
112 efficacy of the kicker to halt this forward momentum may be determined by the strength
113 capabilities of their lower limbs. Although currently unexplored in rugby kicking, previous
114 research investigating the relationship between lower limb strength and kicking velocity in
115 soccer is inconclusive (e.g. Cabri et al. (1988) found a strong positive relationship, Saliba &
116 Hrysomalis (2001) non-significant weak-moderate relationships and Cometti et al. (2001) an
117 unclear relationship), likely due to the common use of isokinetic tests which do not reflect the
118 specific demands of the kicking action (Rodriguez-Lorenzo et al., 2016). Maximal jump tests
119 have also produced conflicting relationships with ball velocity in soccer kicks (three studies
120 identifying a significant relationship and four a non-significant relationship; Rodriguez-
121 Lorenzo et al., 2016), potentially due to the unclear familiarisation procedures employed and
122 the varied experience of players assessed.

123
124 Although there is limited research into how a rugby kicker's approach to the ball may affect
125 place kicking, evidence from other football codes has highlighted how motion during the
126 approach phase can influence ball velocity and thus kick range, and how other factors such as
127 strength and anthropometrics may interact with this. Given the importance placed on the
128 approach phase by coaches, as well as the influence of place kicking success on rugby match
129 outcome, it is crucial to identify practically meaningful aspects that coaches may be able to
130 address in order to improve place kicking range. Therefore, the aim of this study is to
131 understand how a place kicker's approach to the ball affects their performance, and whether
132 physical characteristics influence this.

133 134 **Methods**

135 136 **Participants**

137 Thirty-three male competitive rugby players (mean \pm SD: age = 22 \pm 4 years, mass = 86.2 \pm
138 8.8 kg, height = 1.82 \pm 0.06 m), proficient at place kicking and playing at levels ranging from
139 amateur to senior international, provided written informed consent to participate in this study.

140 The study was approved by the local university research ethics committee prior to testing
141 (reference number: SMEC_2012-13_001).

142

143 **Procedures**

144 All data for each participant were collected in a single testing session, in an indoor laboratory.
145 The order of the procedures was consistent across all participants in that anthropometric data
146 were collected first, then place kicking trials were undertaken, and finally vertical jump tests
147 were conducted. Sufficient, self-selected rest was provided to participants throughout, and they
148 refrained from strenuous physical activity in the 24 hours prior to testing.

149

150 *Anthropometric Measurements*

151 Standing heights were measured using a stadiometer, and mass and leg length (average height
152 of both greater trochanter motion capture markers) were measured during a standing trial on a
153 force platform (9287BA, Kistler, Switzerland; 960 Hz). A Casio EX-FH20 digital camera was
154 used to obtain images (2592 × 3456 pixels) of the participants standing upright in the frontal
155 plane and left and right views of the sagittal plane within a planar six-point calibration frame.
156 Specific anatomical landmarks were digitised (Gittoes et al., 2009) on two separate occasions
157 using Motus (v.9, Vicon, Oxford, UK) and average coordinates of each landmark were
158 reconstructed using 2D Direct Linear Transformation (Abdel-Aziz & Karara, 1971). These data
159 were input to Yeadon's (1990) mathematical model to produce individual-specific segment
160 masses and lengths for the torso, thigh and shank. An average of both limbs was calculated,
161 and segmental lengths were expressed as a percentage of height.

162

163 *Place Kicking Analysis*

164 Following a self-directed warm-up and familiarisation, participants performed a minimum of
165 five place kicks, as if from their maximum range, towards a vertical target (representative of
166 the centre of the goal posts) suspended in a net, 2 m away. Participants wore their own moulded
167 boots and used their preferred kicking tee. Eighty retro-reflective markers (25 mm diameter)
168 were positioned on anatomical landmarks, a headband, wristbands and rigid clusters to define
169 a 14-segment kinematic model during a static trial (described in Atack et al., 2019b and detailed
170 in Supplementary Tables 1 and 2). Fifty-four of these markers remained on the participant
171 during the kicking trials (tracked by a Vicon[®] MX3 system, 240 Hz) along with six circular
172 markers attached to the ball (Gilbert Virtuo, size 5). GRF underneath the support foot was
173 synchronously recorded (960 Hz) using a Kistler 9287BA force platform.

174

175 Marker trajectories were labelled using Nexus v1.8.3 and the .c3d files were exported for
176 processing in Visual 3D (v. 5.0, C-Motion, USA). All trials were cropped one frame pre-BC,
177 identified by the kicking toe marker reaching peak anterior velocity (Shinkai et al., 2009), and
178 marker data were low-pass filtered at 18 Hz using a fourth-order Butterworth filter with
179 endpoints padded (20-point reflection). The raw GRF data were filtered at 125 Hz, with cut-
180 off frequencies identified through residual analysis (Winter, 2009). Segmental kinematics were
181 reconstructed using an Inverse Kinematics global optimisation approach (Lu & O'Connor,
182 1999) with three rotational degrees of freedom at all joints.

183

184 To reduce the dataset and ensure technique characteristics that are practically meaningful to
185 coaches were identified from the data, three key events which align with instants in the
186 movement often focussed on by coaches (Bezodis et al., 2017) were identified from the
187 processed data: kicking foot take-off (KFO), the frame in which the kicking foot toe marker
188 was more than 0.10 m above the ground (Lees et al., 2009) following its final ground contact.
189 Support foot contact (SFC), the frame in which the recorded vertical GRF data first increased,

190 and subsequently remained above, 10 N. Top of the backswing (TB), the frame where the
191 kicking foot CM reached its highest vertical position.

192

193 The participants' whole-body CM location was calculated and CM displacement and velocity
194 time-histories were determined. The whole-body CM position (relative to the ball) and velocity
195 at KFO, SFC and at the instant prior to BC (hereafter, identified as BC) were extracted. The
196 3D displacement of the kicking foot CM at TB relative to the ball CM on the tee was
197 determined. Similarly, the 3D position and velocity of the kicking foot at BC was also
198 measured, and the latter enabled the horizontal and vertical planar angles of the kicking foot
199 path to be determined at BC. The distance between the support foot CM at SFC and the ball
200 CM was also calculated. The length of the final step towards the ball was calculated as the
201 resultant displacement between the kicking foot CM in the frame prior to KFO and the support
202 foot CM at SFC, and the angle of this vector relative to the global antero-posterior axis was
203 calculated. All calculated position and displacement variables were normalised to leg length.

204

205 The recorded GRF data were normalised to body weight (Hof, 1996) before peak values and
206 their timings were extracted. Net impulse was calculated in the three principal directions
207 through integration (trapezium rule) and divided by mass to calculate the deceleration of the
208 whole-body CM in each direction between SFC and BC. Total horizontal deceleration was also
209 calculated.

210

211 To determine the performance of each kick, an aerodynamic model of rugby ball flight was
212 used to obtain the predicted *maximum distance* (Atack et al., 2019a) using the measured initial
213 ball kinematics. The trial in which the participant achieved the greatest predicted *maximum*
214 *distance* was used for subsequent analysis. The reason for failure of that kick from any greater
215 distance was also identified as either "inaccurate" (would have passed outside the goalposts)
216 or "lacking range" (would have dropped below crossbar height).

217

218 *Vertical Jump Tests*

219 After the kicking trials, participants performed six maximal vertical jumps on the force
220 platform. These jumps comprised two squat jumps (SJs), two countermovement jumps (CMJs)
221 and two drop jumps from a 30 cm box (DJs). All jumps were performed with arms folded
222 across the chest. The vertical force data were exported and analysed in Matlab (v.7.12.0, The
223 MathWorks Ltd., USA). Jump heights were calculated from flight times using a 10 N threshold
224 (integration of force data was not possible as not all participants were static prior to initiating
225 the jump, but all maintained extended legs in-flight and landed in this position). The trial where
226 the greatest height was achieved for each jump type was selected for further analysis. Peak
227 propulsive force was normalised to body weight. Reactive strength index (RSI) was calculated
228 for the DJ (Flanagan & Comyns, 2008), modified RSI (RSI_{mod}) was calculated for the CMJ
229 (Ebben & Petushek, 2010), and the Eccentric Utilisation Ratio (EUR) was calculated by
230 dividing the CMJ height by SJ height.

231

232 **Statistical Analysis**

233 Given the aim of this study, the data from the participants whose kicks were deemed to be
234 "lacking range" (n = 17) were retained for further analysis. Participants whose best kick was
235 "inaccurate" were excluded so that this analysis focussed on the movements that limited the
236 range of straight kicks. First, Pearson correlation coefficients were used to assess the
237 relationships between kick performance measures. *Maximum distance* was deemed the primary
238 criterion variable as it encompasses both the distance and accuracy requirements of place
239 kicking. However, as many previous studies have used other measures of performance, such

240 as ball velocity post-contact and kicking foot velocity at BC, it was important to understand
241 the relationships between these variables. Correlation coefficient thresholds were defined as
242 follows: $r < 0.1$ trivial, $0.1 \leq r < 0.3$ small, $0.3 \leq r < 0.5$ moderate and $r \geq 0.5$ strong (Cohen,
243 1988); whilst $p < 0.05$ indicated a significant correlation.
244

245 As multiple constructs (namely technique characteristics, strength capabilities and
246 anthropometric parameters) each containing numerous variables were investigated, principal
247 component analysis (PCA) was used to reduce the number of variables analysed (as previously
248 performed by Ball, 2008 and Colyer et al., 2017). To ensure the PCA had sufficient power
249 despite the inevitable small sample size associated with collecting data in specialist sport
250 contexts, an initial selection of variables to be included was undertaken. Following Hair et al.'s
251 (2009) recommendation, first, the variables were assessed based on their association with the
252 criterion performance measure of *maximum distance* and any variables with strong significant
253 correlations were extracted. Subsequently only variables that were deemed to be independent
254 of the others were selected for inclusion (e.g. if all individual components and the composite
255 variable were identified, the composite was selected but if only individual components were
256 identified these were used for subsequent analysis).
257

258 All variables selected for inclusion in the PCA were then transformed into z-scores to
259 standardise scaling for analysis in SPSS Statistics (v.24; IBM Corp, Armonk, NY). The Bartlett
260 test of sphericity and Kaiser-Meyer-Olkin measure of sampling adequacy were used to confirm
261 the suitability of the dataset for PCA. An initial solution was computed with the optimum
262 number of components identified when the Cumulative Initial Eigenvalues totalled more than
263 90% (Jolliffe, 2002). An orthogonal varimax rotation was used to simplify the structure. A
264 significant loading was identified if more than ± 0.7 loading was seen on a single component,
265 and any variables which were loaded across multiple components were eliminated. Labels were
266 assigned to describe each component, reflecting all of the variables with significant loading.
267

268 The variable demonstrating the strongest relationship to each component was considered to
269 represent the broad component and used as a predictor variable in a stepwise multiple
270 regression analysis to determine place kick performance. Initially, *maximum distance* was used
271 as the criterion for the regression before it was repeated using the other performance
272 components that were strongly correlated to *maximum distance* to identify how these variables
273 also related to the ball launch velocity attained as well as the foot velocity at BC. The Durbin-
274 Watson statistic assessed autocorrelation, and the consistency of the residuals were evaluated
275 using the Breusch-Pagan and Koenker homoscedasticity tests (Breusch & Pagan, 1979;
276 Koenker & Bassett, 1982) and standard normality tests. Entered variables remained in the
277 regression model if they elicited a significant R^2 change ($p < 0.05$).
278

279 A K -fold leave-one-out cross-validation method was used to assess the stability of the
280 predictive regression models. The standard error of measurement (SEM) was calculated
281 between the performance variables predicted by the cross-validation and the measured values,
282 and correlations between the two datasets were analysed, with the R^2 value compared to the
283 initial model.
284

285 Results

286
287 *Bivariate correlations to assess the relationship of performance components with maximum*
288 *distance*
289

290 The 17 analysed kicks had a *maximum distance* of 37.19 ± 7.48 m (range = 21.8-53.3 m).
 291 Analysis of the initial in-flight ball kinematics and the kicking foot kinematics at BC revealed
 292 strong, significant correlations between a number of variables and the *maximum distance* of
 293 the kicks (Table 1). Resultant ball launch and kicking foot velocity showed the strongest
 294 correlations with *maximum distance* (both $r = 0.81$), whilst components of these (antero-
 295 posterior and vertical ball velocity, and medio-lateral and antero-posterior foot velocity) were
 296 also strongly correlated ($r = 0.80, 0.63, 0.79$ and 0.60 respectively). Therefore, the two resultant
 297 velocities and the lateral direction of the kicking foot velocity vector in the horizontal plane at
 298 BC (hereafter termed ‘lateral direction of the kicking foot’; $r = 0.69$) were identified as the
 299 variables which best determined the *maximum distance* of the kicks and were subsequently
 300 used as additional dependent variables in the regression analyses.
 301

Table 1. The measured initial ball flight and the kicking foot kinematic variables at ball contact, and their respective Pearson correlation coefficients ($\pm 95\%$ CL) with the *maximum distance* of the kick.

	mean \pm sd	Relationship with <i>maximum distance</i>	
		r ($\pm 95\%$ CL)	p value
Ball Flight Kinematics			
Resultant launch velocity (m/s)	26.05 \pm 3.49	0.81 (0.53 – 0.93)	<0.001
Lateral velocity component (m/s)	0.38 \pm 0.88	-0.22 (-0.62 – 0.28)	0.391
Anterior velocity component (m/s)	21.99 \pm 3.35	0.80 (0.51 – 0.92)	<0.001
Vertical velocity component (m/s)	13.86 \pm 1.75	0.63 (0.21 – 0.85)	0.006
End-over-end angular velocity ($^{\circ}$ /s)	2173 \pm 985	0.27 (-0.24 – 0.65)	0.297
Yaw angular velocity ($^{\circ}$ /s)	-9 \pm 520	-0.18 (-0.59 – 0.32)	0.500
Longitudinal angular velocity ($^{\circ}$ /s)	305 \pm 270	-0.44 (-0.75 – 0.05)	0.080
Lateral launch direction ($^{\circ}$)	1 \pm 3	-0.33 (-0.69 – 0.17)	0.196
Vertical launch direction ($^{\circ}$)	32 \pm 3	-0.38 (-0.72 – 0.12)	0.131
Kicking Foot CM Kinematics at Ball Contact			
Resultant velocity (m/s)	19.46 \pm 1.82	0.81 (0.52 – 0.92)	<0.001
Lateral velocity magnitude (m/s)	7.67 \pm 2.18	0.79 (0.40 – 0.91)	<0.001
Anterior velocity magnitude (m/s)	17.61 \pm 1.43	0.60 (0.16 – 0.83)	0.012
Vertical velocity magnitude (m/s)	-2.37 \pm 0.89	-0.22 (-0.62 – 0.28)	0.392
Lateral direction ($^{\circ}$)	23 \pm 6	0.69 (0.31 – 0.87)	0.002
Vertical direction ($^{\circ}$)	-8 \pm 3	-0.11 (-0.55 – 0.38)	0.673

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Bivariate correlations to assess the relationship of technique characteristics, strength capabilities and anthropometric parameters with maximum distance

A large number of strong, significant correlations were also identified between *maximum distance* and variables which described the kickers’ approach to the ball (CM kinematics, Figure 1; final step kinematics, Figure 2), the position of the kicking foot at TB (Figure 3) and the jump performance measures (Figure 4). However, no strong correlations were observed with the GRFs exerted under the support foot during the place kicks (Figure 5) or the kickers’ anthropometric characteristics (Figure 6). Fifteen variables (those in bold in Figures 1-6) were entered into the PCA as they were all strongly correlated with *maximum distance* and were deemed independent of each other.

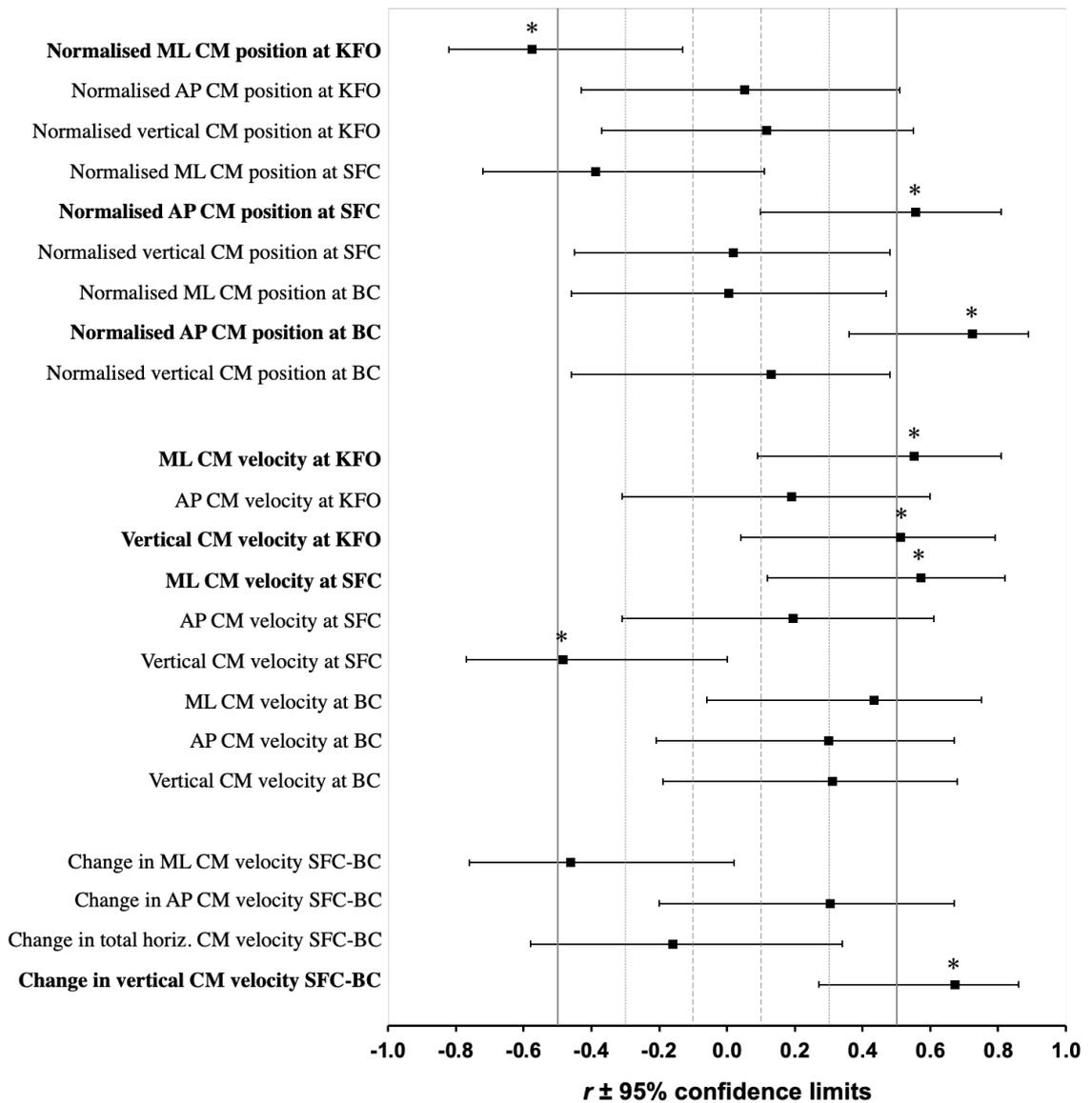


Figure 1. Pearson correlation coefficients (\pm 95% CL) between *maximum distance* and centre of mass kinematics prior to ball contact. Negative coefficients for the medio-lateral positions represent being to the left of the ball. Solid grey vertical lines indicate a strong correlation ($r = 0.5$), dotted lines a moderate correlation ($r = 0.3$) and dashed lines a weak correlation ($r = 0.1$). * denotes a significant correlation ($p < 0.05$). Abbreviations: ML, medio-lateral; AP, antero-posterior; CM, centre of mass; KFO, kicking foot take-off; SFC, support foot contact; BC, ball contact.

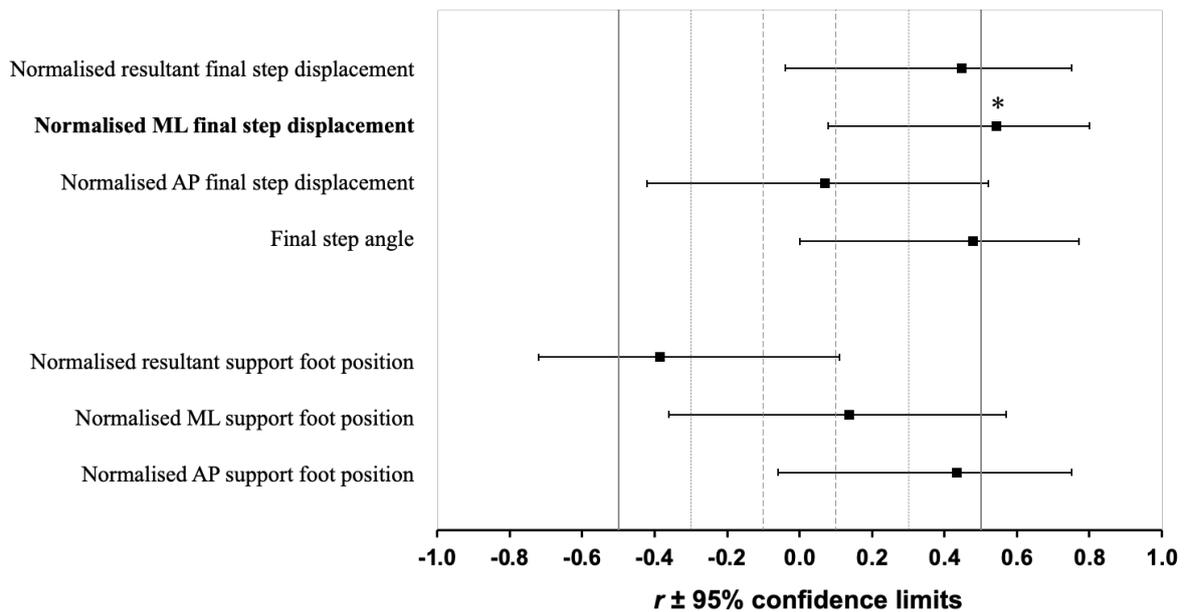


Figure 2. Pearson correlation coefficients (\pm 95% CL) between *maximum distance* and normalised final step kinematic variables. Negative coefficients for the medio-lateral positions represent being to the left of the ball. Solid grey vertical lines indicate a strong correlation ($r = 0.5$), dotted lines a moderate correlation ($r = 0.3$) and dashed lines a weak correlation ($r = 0.1$). * denotes a significant correlation ($p < 0.05$). Abbreviations: ML, medio-lateral; AP, antero-posterior.

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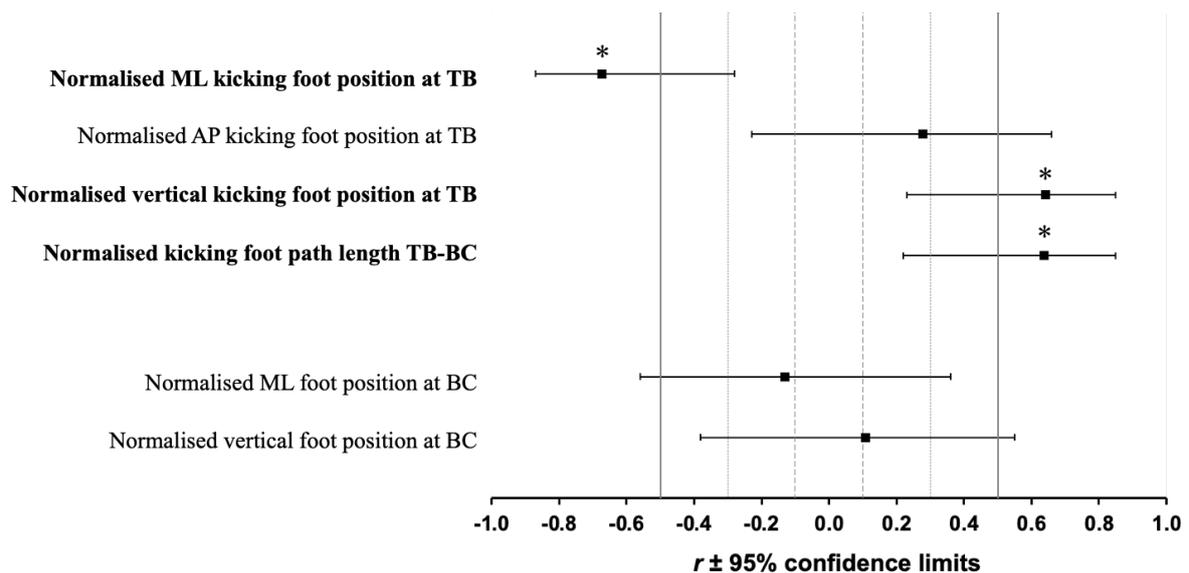


Figure 3. Pearson correlation coefficients (\pm 95% CL) between *maximum distance* and kicking foot kinematics during the downswing. Negative coefficients for the medio-lateral positions represent being to the left of the ball. Solid grey vertical lines indicate a strong correlation ($r = 0.5$), dotted lines a moderate correlation ($r = 0.3$) and dashed lines a weak correlation ($r = 0.1$). * denotes a significant correlation ($p < 0.05$). Abbreviations: ML, medio-lateral; AP, antero-posterior; TB, top of the backswing; BC, ball contact.

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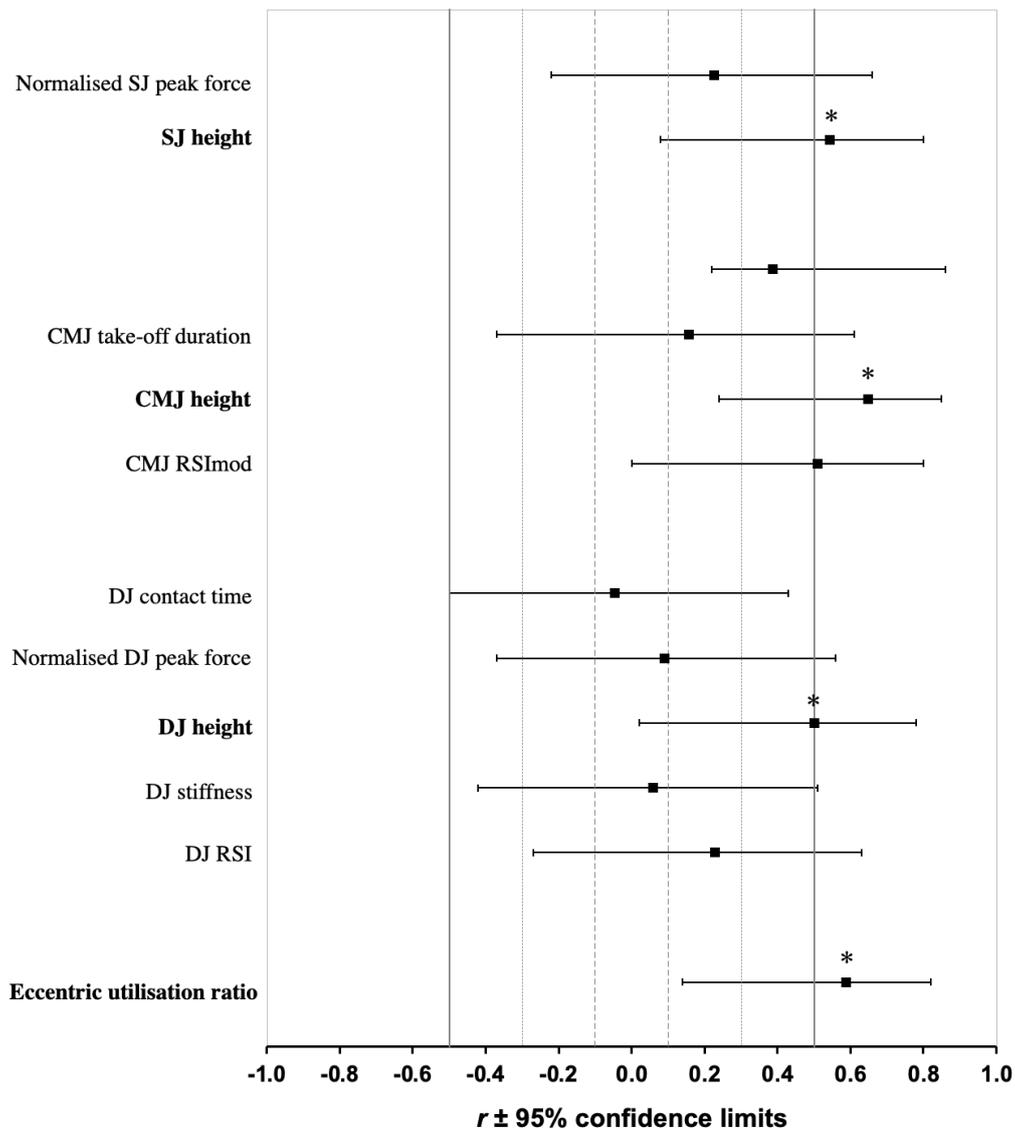


Figure 4. Pearson correlation coefficients (\pm 95% CL) between *maximum distance* and jump performance characteristics. Negative coefficients for the medio-lateral positions represent being to the left of the ball. Solid grey vertical lines indicate a strong correlation ($r = 0.5$), dotted lines a moderate correlation ($r = 0.3$) and dashed lines a weak correlation ($r = 0.1$). * denotes a significant correlation ($p < 0.05$). Abbreviations: SJ, squat jump; CMJ, countermovement jump; DJ, drop jump; RSI, reactive strength index.

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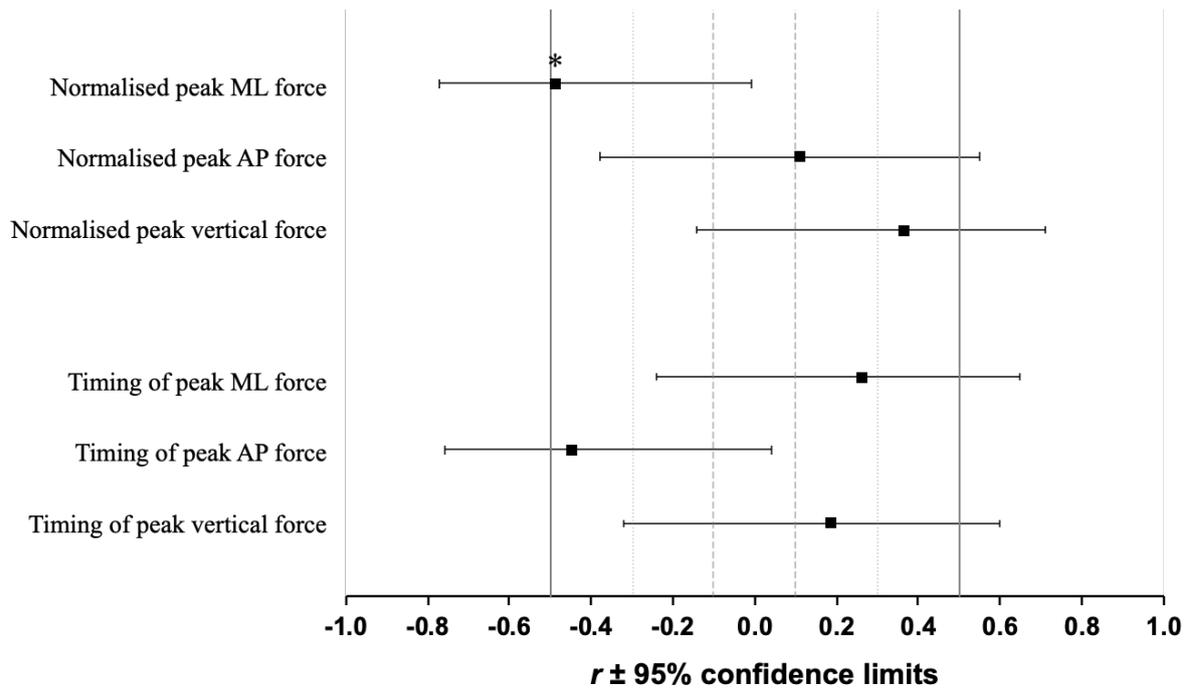


Figure 5. Pearson correlation coefficients (\pm 95% CL) between *maximum distance* and ground reaction forces exerted underneath the support foot. Negative coefficients for the medio-lateral positions represent being to the left of the ball. Solid grey vertical lines indicate a strong correlation ($r = 0.5$), dotted lines a moderate correlation ($r = 0.3$) and dashed lines a weak correlation ($r = 0.1$). * denotes a significant correlation ($p < 0.05$). Abbreviations: ML, medio-lateral; AP, antero-posterior.

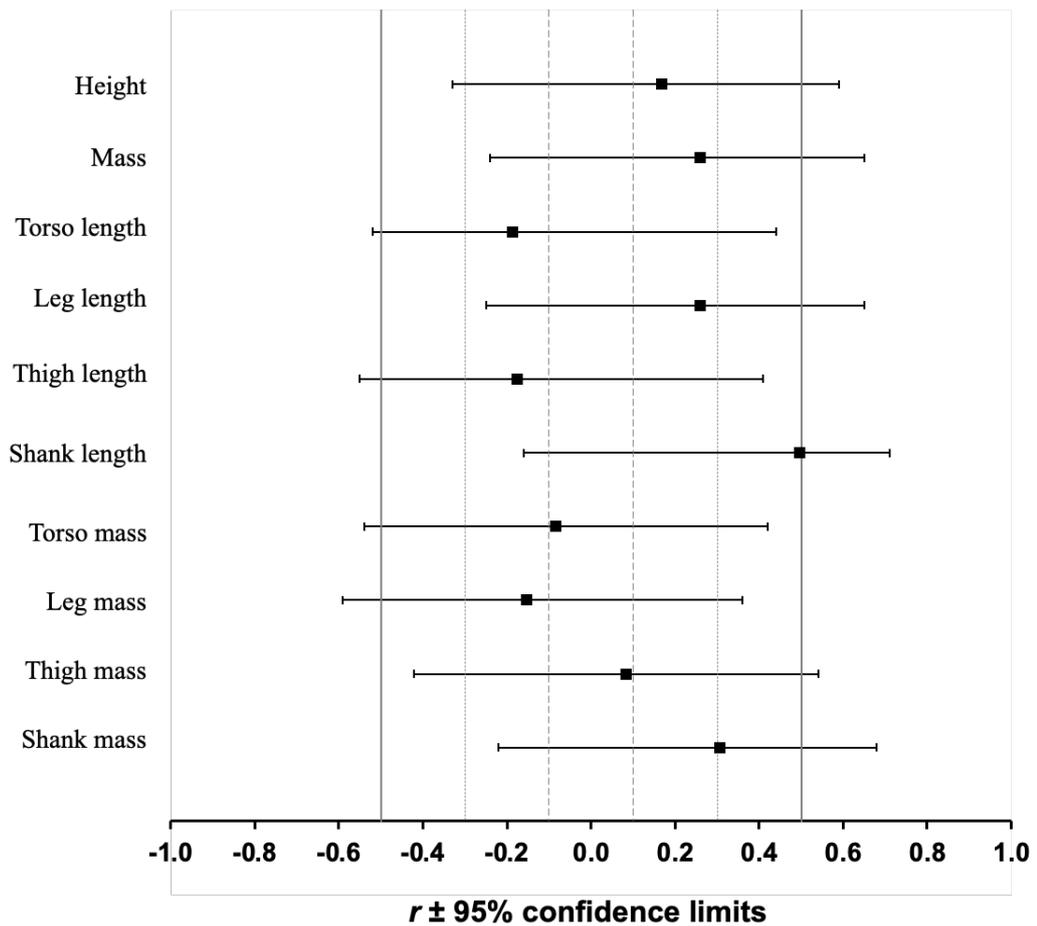


Figure 6. Pearson correlation coefficients (\pm 95% CL) between *maximum distance* and anthropometric characteristics of the kickers. Negative coefficients for the medio-lateral positions represent being to the left of the ball. Solid grey vertical lines indicate a strong correlation ($r = 0.5$), dotted lines a moderate correlation ($r = 0.3$) and dashed lines a weak correlation ($r = 0.1$). * denotes a significant correlation ($p < 0.05$).

323 *Components and loading of variables derived from PCA*

324

325 Following the first iteration of the PCA, three variables (change in vertical CM velocity from
 326 SFC to BC, kicking foot path length from TB to BC and EUR) were cross-loaded across
 327 multiple components and thus eliminated prior to re-running the analysis. The variables
 328 included in the second iteration met all conditions (each had a significant loading on a single
 329 component) and the Kaiser-Meyer-Olkin measure of sampling adequacy (0.700) and the
 330 Bartlett's test of sphericity ($p < 0.001$) confirmed that the data were appropriate for the analysis.
 331 Four components were extracted from the PCA (Table 2), explaining 94% of the variance in
 332 the data. The components were interpreted to represent: 1, width of approach; 2, anterior-
 333 posterior body position; 3, CM height; 4, lower limb strength.

334

Table 2. Components identified from the Principal Component Analysis and the corresponding loading of each variable to the components.

	Component			
	1	2	3	4
ML CM position at KFO	-0.923	-0.165	-0.170	-0.186
ML CM velocity at KFO	0.916	0.208	-0.066	0.292
ML CM velocity at SFC	0.898	0.211	-0.091	0.314
ML kicking foot position at TB	-0.874	-0.311	-0.302	-0.169
ML final step displacement	0.909	0.186	0.203	0.230
AP CM position at SFC	0.522	0.795	0.054	-0.139
AP CM position at BC	0.203	0.913	0.145	0.255
Vertical CM velocity at KFO	-0.044	0.035	0.876	0.386
Vertical kicking foot position at TB	0.475	0.290	0.703	0.279
CMJ Height	0.310	0.171	0.289	0.870
SJ Height	0.191	0.096	0.208	0.934
DJ Height	0.298	-0.018	0.208	0.869

335 Abbreviations: ML, medio-lateral; AP, antero-posterior; CM, centre of mass; KFO, kicking foot take-
336 off; SFC, support foot contact; TB, top of the backswing; BC, ball contact; CMJ, countermovement
337 jump; SJ, squat jump. Variable names in bold (with values shaded) used to represent the individual
338 components in the multiple regression analysis.

339

340 *Stepwise regression analyses to determine the predictors of place kick performance*

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342 The variables with the greatest loading to each component (shaded values in Table 2) were
343 medio-lateral CM position at KFO (1), antero-posterior CM position at BC (2), vertical CM
344 velocity at KFO (3) and SJ height (4). When entered into a stepwise multiple regression model,
345 two of these (antero-posterior CM position at BC and vertical CM velocity at KFO) were found
346 to explain 64% of the total variance in the *maximum distance* of the place kicks (Table 3). The
347 same four predictor variables were entered into separate stepwise multiple regression models
348 to predict resultant ball launch velocity, resultant kicking foot velocity and lateral direction of
349 the kicking foot at BC as these represent the performance criteria that were strongly associated
350 with *maximum distance*. These further the understanding of how performance was achieved
351 and were able to explain 71%, 55% and 71% of the total variance in the respective dependent
352 variables (Table 3).

Table 3. Results and validation data for the stepwise multiple regression models to estimate the *maximum distance* of the place kicks and other associated performance criteria.

Dependent Variable	Regression equation components			Variance explained (R^2 , p value)		Model assessment statistics				
	Independent variable 1 (unstandardised β coefficient)	Independent variable 2 (unstandardised β coefficient)	Constant	Independent variable 1	Independent variable 2	Durbin-Watson statistic	Breusch-Pagan (p value)	Koenker (p value)	K-fold validation	
									Correlation of predicted values and measured (R^2 , p value)	SEM
<i>Maximum distance</i>	AP CM position at BC (0.449)	vertical CM velocity at KFO (13.149)	42.294	0.52 $p = 0.001$	0.12 $p = 0.049$	1.972	0.524	0.426	0.50 $p = 0.002$	4.54 m
Resultant ball launch velocity	SJ height (28.67)	ML CM position at KFO (-0.083)	7.15	0.57 $p < 0.001$	0.14 $p = 0.024$	1.840	0.524	0.426	0.56 $p = 0.001$	1.83 m/s
Resultant kicking foot velocity	SJ height (18.727)	-	12.418	0.55 $p = 0.001$	-	1.573	0.256	0.192	0.46 $p = 0.003$	0.98 m/s
Lateral direction of kicking foot	ML CM position at KFO (-0.199)	AP CM position at BC (0.237)	8.513	0.56 $p = 0.001$	0.15 $p = 0.016$	1.723	0.524	0.426	0.59 $p < 0.001$	3°

Abbreviations: ML, medio-lateral; AP, antero-posterior; CM, centre of mass; BC, ball contact; KFO, kicking foot take-off; SJ, squat jump; SEM, standard error of measurement.

Discussion

We explored the association between the kickers' approach to the ball, their physical characteristics and rugby place kicking performance. Using PCA we identified four components which explained 95% of the variance in the *maximum distance* place kickers can achieve. These four components categorised 1) width of approach, 2), anterior-posterior body position 3) height of the CM and 4) lower limb strength, highlighting the importance of considering the three-dimensional motion of the kickers' approach to the ball and their physical capabilities. The variables which best represented each component were 1) medio-lateral CM position at the final kicking foot take-off prior to ball contact, 2) antero-posterior CM position at ball contact, 3) vertical CM velocity at the final kicking foot take-off prior to ball contact and 4) squat jump height. Each of these variables were retained in either the regression model that predicted overall performance (*maximum distance*) or one of the models that predicted the other associated performance criteria (resultant ball velocity magnitude, kicking foot velocity magnitude or lateral direction of the kicking foot). In order to develop the understanding of successful overall performance, we will first consider how favourable kicking foot velocity (both magnitude and direction) at ball contact is achieved, then ball launch velocity, and finally *maximum distance*.

The kicking foot is the distal end of the linked segment system which contacts the ball, determines its flight post-contact and ultimately kick distance. The resultant kicking foot velocity magnitude demonstrated a strong relationship with *maximum distance* ($r = 0.81$, $p < 0.001$), as previously reported in Australian Rules punt kicking for distance (Ball, 2008). Lower-limb strength was the sole significant predictor of the variance in resultant kicking foot velocity magnitude (explaining 55% of the total variance). Given the weak-moderate correlations between *maximum distance* and the recorded GRFs and change in horizontal CM velocity during support foot contact, increased strength does not appear to influence a kicker's ability to brake their forward momentum. Instead, greater lower limb strength could facilitate positive lower limb joint work during the downswing and subsequently the velocity of the kicking foot. Thus, greater lower limb concentric strength as evidenced through increased SJ height, is likely reflective of increased capacity of the knee extensors (Luhtanen & Komi, 1979) which can then be utilised to achieve faster kicking foot velocities (Atack et al., 2019b). Although previous research has presented contradictory findings as to the relationship between lower-limb strength and kicking performance in other football codes (e.g. Cabri et al., 1988; Cometti et al., 2001), the use of isokinetic dynamometry or squat tests are a likely reason as they do not adequately reflect the knee extension velocities observed during the downswing of a place kick ($>1000^\circ/s$). Those studies which did employ explosive tests, such as maximal jumps, tended to identify stronger correlations but may also have been impacted by the varied experience of the participants and the lack of familiarisation provided.

In addition to kicking foot velocity magnitude, it is also important to consider the direction of the foot velocity vector given the importance of an appropriate ball trajectory in rugby place kicking (Atack et al., 2019a). We found the lateral direction of the kicking foot velocity vector in the horizontal plane at BC was strongly correlated with *maximum distance* ($r = 0.69$, $p = 0.002$). Whilst lower limb strength is important in determining the magnitude of the kicking foot velocity, it is the position of the body that determines its direction - width of approach and antero-posterior body position combined to explain 71% of its variance. Although experimental manipulations to approach angle have produced equivocal findings in terms of ball velocity magnitude (Kellis et al., 2004; Isokawa & Lees, 1988; Scurr & Hall, 2009), the effect on the direction of the kicking foot or ball velocity is previously unexplored as these studies have not

406 considered kick accuracy. Analysis of the variables loaded to these two components highlights
407 the importance of adopting a wider approach earlier in the kicking phase (i.e. at kicking foot-
408 take off to support foot contact) but a more anterior position later in the phase (from support
409 foot contact to ball contact). Therefore, the inclusion of these components in this model
410 suggests that the two factors combine to influence the kicking foot swing plane during the
411 downswing and ultimately the foot velocity direction at BC. Although previous research
412 (Bezodis et al., 2019) has identified differences in both the inclination and direction of the
413 kicking foot swing planes of accurate and inaccurate place kickers, such an analysis has not
414 been conducted across solely those who are limited by their range. An observed difference in
415 this swing plane may explain how different foot-ball collisions are achieved and the subsequent
416 effect this can have on ball flight. Thus, in order to understand the effect of these two factors
417 (a wider approach and a more forward body position) on the range achieved by accurate rugby
418 union place kickers, further analysis of kicking foot swing planes alongside the foot-ball
419 interaction is warranted.

420

421 As expected, resultant ball velocity magnitude demonstrated a strong relationship with
422 *maximum distance* ($r = 0.81$, $p < 0.001$). The regression model for resultant ball velocity
423 included two of the components identified in the models describing kicking foot motion. Lower
424 limb strength combined with the width of the approach to explain 71% of the total variance.
425 Given lower limb strength was the sole significant predictor of resultant kicking foot velocity
426 and the strong relationship observed between resultant foot and ball velocities in a range of
427 football codes ($r = 0.68 - 0.83$; Ball, 2008; De Witt & Hinrichs, 2012; Nunome et al., 2006),
428 the importance of lower limb strength in achieving a fast ball velocity is clear. The inclusion
429 of a wider approach in the model is of interest given the previously identified relationship it
430 has with the direction of the kicking foot velocity vector at BC and the equivocal findings in
431 the literature when approach angle was experimentally manipulated (Kellis et al., 2004;
432 Isokawa & Lees, 1988; Scurr & Hall, 2009). Participants in the present study approached from
433 a mean angle of 49° (range $36-66^\circ$), which is comparable to the 45° previously found to elicit
434 the fastest mean ball velocities in soccer instep kicking. Isokawa and Lees (1988) suggested a
435 more angled approach may enable a greater effective mass of the foot due to the player adopting
436 a more rigid ankle joint, thereby increasing coefficient of restitution during impact. This is
437 supported by research investigating impact efficiency using a mechanical kicking leg which
438 found that increased simulated ankle rigidity enabled a more efficient collision and
439 subsequently faster ball velocities (Peacock & Ball, 2018). A more proximal impact location
440 on the kicking foot has also been found to reduce the amount of plantarflexion at a mechanical
441 ankle joint resulting in a greater coefficient of restitution and ball velocity compared with a
442 more distal impact location (Peacock & Ball, 2019). Therefore, we propose that it is not an
443 angled approach that enables a faster ball velocity to be achieved *per se*, but that the greater
444 lateral distance of the kicker from the ball at the initiation of kicking leg retraction allows them
445 more space for the downswing, altering the direction of the foot velocity vector and enabling a
446 more efficient foot-ball collision. High-speed analyses of the impact phase of rugby place kicks
447 are required to directly investigate this, and these findings must also currently be applied with
448 caution as it is possible that approaching from too great an angle or achieving too great a lateral
449 distance from the ball could negatively affect other key technical features and thus an optimum
450 may exist. Furthermore, the relative importance of different variables and the existence or
451 location of optima are likely to differ between individuals. Any interventions to address these
452 aspects should therefore be applied on an individual-specific basis and with an awareness of
453 other potential consequences, whilst kickers with 'extreme' technique features should be
454 considered with caution as they may fall outside the ranges studied in the current cohort.

455

456 Although the magnitude and direction of the kicking foot velocity and the magnitude of ball
457 velocity are associated with rugby place kick performance, these alone do not determine overall
458 place kick success (Atack et al., 2019a). Therefore, to complete our understanding it is vital to
459 consider the factors that contribute to true place kick performance outcome, namely *maximum*
460 *distance*. The antero-posterior body position and CM height explained 64% of the variance in
461 *maximum distance*. First to note, is that whilst lower limb strength was a significant predictor
462 of both foot and ball velocity magnitudes, its omission from this final regression suggests that
463 although lower limb strength is important in achieving fast kicking foot and ball speeds, the
464 position and motion of the CM ultimately differentiates the overall true performance outcome.
465 Secondly, the antero-posterior body position of the kicker was earlier identified as important
466 in determining the direction of the kicking foot velocity vector, potentially through alterations
467 to the kicking foot swing plane. Further to this, by positioning their body further forward, and
468 closer to the ball, the kicking foot will likely be in a lower position on its downward path and
469 therefore can contact the ball towards the more proximal end of the foot resulting in a more
470 efficient foot-ball collision, thereby influencing ball flight. Finally, this is the first model that
471 has included CM height as a significant predictor. Augustus et al. (2017) previously suggested
472 that raising the support leg hip enabled greater transfer of momentum to the kicking foot and
473 subsequently a faster ball velocity in soccer kicking. However, as vertical CM motion was not
474 included in the previous regression model for ball velocity magnitude, it is suggested that
475 raising the CM earlier in the approach likely contributes to place kicking performance in
476 another way. If we consider the variable used to represent CM height in this regression, vertical
477 CM velocity at kicking foot take-off, kickers who have a faster velocity (and subsequently
478 greater height into the final step), will also have greater downward velocity at support foot
479 contact. If they are then able to absorb this downward momentum and use it to rebound through
480 the kicking action, they may be able to achieve a more favourable ball flight. The ability to
481 rebound would likely be reflected by an increased EUR or a greater change in vertical velocity
482 following support foot contact. Both these variables were identified as strongly correlated to
483 *maximum distance* but were removed from the PCA after the first iteration due to cross-loading
484 over multiple components. Given neither the antero-posterior body position or CM height were
485 included in the model that explained the variance in ball velocity magnitude, it may be that
486 they instead affect another aspect of ball flight post-contact such as the vertical launch
487 direction. The variance in vertical launch direction was not investigated as an associated
488 performance measure, as only a moderate linear relationship was identified with *maximum*
489 *distance*. Previous research identified a non-linear (cubic) relationship between vertical launch
490 direction and kick distance for an individual place kicker (Linthorne & Stokes, 2014), and
491 although such a relationship was not apparent in the present study, future research should
492 consider the factors that may contribute to this aspect of ball flight.

493
494 In conclusion, several aspects describing both the kicker's approach to the ball and their
495 physical capabilities that are meaningful to coaches were found to influence place kick
496 performance. Lower limb strength appears important for a kicker to achieve a fast kicking foot
497 velocity, whilst taking a wider approach and adopting a more anterior body position (closer to
498 the ball) affect the direction of the kicking foot's motion at BC. A combination of these factors
499 (greater lower limb strength and a wide approach) is subsequently required to achieve a fast
500 ball velocity. However, CM height and the anterior-posterior body position of the kicker
501 ultimately determines the maximum range of accurate place kickers. Replication of the present
502 study with a different sample population is suggested to assess the robustness of these findings.
503 Additionally, the specific mechanisms by which increased kicking range is achieved requires
504 further investigation, particularly in terms of the detail of the foot-ball impact which is
505 currently unexplored in place kicking but appears vital in determining overall performance.

506

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508

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511

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513

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515

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517

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519

520 **Data availability statement**

521

522 The data that support the findings of this study are available from the corresponding author
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524 **References**

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